

United States Patent Application

of

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for

METHOD FOR USING A PRE-JEL FOR PRODUCING SELF-REDUCING  
AGGLOMERATES

## BACKGROUND OF THE INVENTION

The present invention relates to self-reducing agglomerates for use in the production of iron, and to methods and apparatus for the production thereof.

The development of iron bearing agglomerates began in the fifties. These agglomerates were mainly in the form of pellets, with the purpose of enabling the use of mineral fines, which the conventional methods, such as those used in blast furnaces, cupola furnaces, electric furnaces and others, could not accept as raw materials due to the fine size thereof, particularly in the case of iron ore. Some time thereafter the development of self-reducing agglomerates began. This development was characterized by the use of cold cure binders, particularly cement, lime and silica, which exhibit as the cure mechanism, mainly reactions with water (hydration) and in lesser amount with the carbon dioxide present in the air (carbonation). Those reactions, although imparting to the agglomerate the desired mechanical properties, are slow reactions, requiring between 10 to 30 days for completion, and sometimes even more depending on the weather conditions (the cure velocity diminishes with the decrease of the ambient temperature).

Some alternatives were developed to accelerate the hydration reactions referred to above, by means of treatment of the agglomerates in pressure vessels (autoclaves) by applying pressures on the order of up to 20 atmospheres and water vapor at 250° C, as recited in US Patent No. 4,528,029, which is incorporated herein. The major disadvantage of this alternative practice is the high cost of the equipment required and the complex operating conditions, rendering the commercial application thereof difficult.



The conveying equipment may include a perforated belt allowing passage of the hot gas therethrough to the agglomerates.

The method according to the invention may comprise the step of forming the agglomerate in the shape of pellets or briquettes or any other suitable geometric shape.

The method according to the invention may employ fluxing materials, such as lime, limestone, steel plant slag, blast furnace slag and similar materials, to flux the nonmetallic impurities present in the agglomerate.

In the method according to the invention, the pre-gel is added to develop the mechanical properties of the agglomerate, particularly the compression strength thereof, upon curing at temperatures in the range from about 100 to about 180°C.

The equipment according to the invention may include a system for the uniform distribution of hot gasses along the belt.

The equipment according to the invention, the heated gas may comprise air, burned gas, water vapor, inert gas and mixtures thereof without restrictions to proportions.

The equipment according to the invention may comprise a plurality of overlapping belt segments in the same direction or with alternately opposed directions of movement.

The equipment according to the invention may include a uniform exhaust system that does not affect the distribution of the heated gasses through ports distributed along the belt.

The heating of the agglomerates to provide drying and curing may be effected using heated air, burned gas, water vapor, inert gas and mixtures thereof, without

restriction in terms of proportions, distributed along the belt to enable the same to pass uniformly through the agglomerates and not interfere with the distribution of the inflow of the heated gas. This avoids the occurrence of preferential gas flow and excessive variation of the uniformity of drying and curing. Hence, the speed of the belt may be constant while providing the required agglomerate residence time for adequate curing.

After the passage of the agglomerates through the curing equipment, the same are ready for use for the metal production.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a longitudinal section view of one embodiment of equipment in accordance with the invention.

Figure 2 is a top view of the equipment of Figure 1.

Figure 3 is a cross sectional view of the equipment of Figure 1.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The self-reducing agglomerates described herein may be cured and dried in the equipment illustrated in Figures 1, 2 and 3. This equipment comprises one or more perforated conveyor belts 1, the speed of which may be controlled to allow an agglomerate residence time between 10 and 60 minutes, more specifically between 20 and 40 minutes. The equipment also has an inlet system 2, for supplying heated gasses at a temperature between 100 and 180° C. It also has an exhaust system 3 for the exhaust of the gasses passing from the agglomerates. One inlet 4 for non-cured

agglomerates and at least one outlet 5 for cured and dry agglomerates, which may thereafter be processed in reducing/melting equipment to produce metals.

The equipment described above cures the agglomerates which are then ready for use in a reducing/melting unit.

The pre-gel is a modified starch that, when submitted to temperatures of about 100 to about 180° C for periods of time between about 10 and about 60 minutes, imparts mechanical properties to the agglomerate, particularly compression strength, at least equivalent to those obtained with the hydraulic cure agglomerates. Additionally, the use of the pre-gel eliminates the need to use specific equipment such as gas pressure vessels, commonly termed as autoclaves.

In accordance with the invention, agglomerates in the form of pellets were produced from a mixture of iron containing material constituting iron ore fines, a reducing agent constituting coal fines and a pre-gel having starch as the major component. Approximately 8% water was added to this mixture to facilitate forming of green pellets. The green pellets were cured by heating for the times at a temperature set forth in Table 1. Upon completion of curing the pellets were tested to determine the cold compression strength thereof by measuring the maximum compressive load on the pellet upon fracture. The results of these tests are set forth in Table 1.

TABLE 1					
Pellet Diameter	Curing Temp.	Curing Time	Pre-gel	Cold Compression Strength	Specified Cold Compression Strength
mm	°C	minutes	%	kgf/pellet	kgf/pellet
11	130	60	1.0	19.46	>15
11	130	60	1.5	17.77	>15
12	140	30	1.5	23.54	>17
13	140	30	0.8	21.86	>20
12	140	60	1.0	23.0	>17
12	150	60	0.8	31.16	>17
12	140	30	3.0	23.97	>17
12	130	0	2.5	21.96	>17

kgf means kilograms of force.

For purposes of the invention, the pre-gel for use therein is defined as a starch modified by temperature and pressure treatment wherein water is initially added and then removed to gelatinize the starch. The gelatinized starch is then ground to fine particle size for use as a binder. The term perforated belt as used therein includes any belt having openings suitable to allow the passage of gas therethrough to the agglomerates on the belt; this would include a belt made of mesh material.